# **Detection of cell cracks and increased series resistance** of crystalline silicon PV modules by using the voltage and current at maximum power point

Manit Seapan<sup>1</sup>, Yoshihiro Hishikawa<sup>2</sup>, Masahiro Yoshita<sup>2</sup>, Keiichi Okajima<sup>1</sup>

1 Department of Risk Engineering, University of Tsukuba 2 Renewable Energy Research Center, AIST

## **Research purpose**

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- Degradations and failures occur in PV modules during their outdoor operation, such as cell cracks and an increase in series resistance  $(R_s)$ .
- Previous detection techniques, such as *I*–*V* curve measurement, had a problem because they needed to interrupt the system operation.

## **Temperature correction of** $V_{mp}$ and $I_{mp}$

The measured  $V_{\rm mp}$  and  $I_{\rm mp}$  are corrected to 25 °C using Eqs. (1) and (2) [1], as shown in Fig. 1.

$$V_{\rm mp2} = \left[ V_{\rm mp1} + \frac{T_2 - T_1}{T_1} \left( V_{\rm mp1} - \frac{nE_{\rm g}}{q} \cdot N_{\rm c} \right) \right] \times \left[ 1 + \alpha (T_2 - T_1) \right], \quad (1)$$

$$I_{\rm mp2} = I_{\rm mp1}.$$



- This study utilizes the temperature corrected of current-voltage at maximum power  $(I_{mp}-V_{mp})$  curve instead of the *I*-V curve using the new formulas recently proposed [1].
- Cracked cell and increase in  $R_s$  were investigated by simulations for detecting degradation using  $I_{\rm mp}$ - $V_{\rm mp}$  curve.

Here,  $T_1$  and  $T_2$  is the measured and target module temperature in Kelvin (K), respectively.  $V_{mp1}$  and  $V_{mp2}$  are the  $V_{mp}$  at  $T_1$  and  $T_2$ , respectively.  $E_g$ is the bandgap energy of silicon. n is the diode ideality factor, q is the electron charge,  $N_c$  is the number of series-connected cells, and  $\alpha$  is the temperature coefficient (TC) of the short-circuit current ( $I_{sc}$ ).  $\alpha$  is estimated to have a value of 0.05%/K .  $I_{\rm mp1}$  and  $I_{\rm mp2}$  are the  $I_{\rm mp}$  at  $T_1$  and  $T_2$ , respectively.  $nE_g/q$  is estimated to have a value of approximately 1.232 V.

Fig. 1 Measured  $I_{\rm mp}$  and  $V_{\rm mp}$  are shown by the black symbols. The red symbols show the curve corrected to 25 °C using Eqs. (1) and (2).

## Cell crack and effect of $R_s$

#### Cell crack

Numerical simulation has been performed to investigate the possible detection of cell cracks using the  $I_{\rm mp}-V_{\rm mp}$  curve. A cracked cell is represented by a cell with a reduced active area, as shown in Fig. 2.

The output current of a silicon PV cell for simulation is expressed by the Bishops model [2] as follows:

 $I = I_{\rm ph} - I_0 \left[ \exp^{\left(\frac{q(V+IR_{\rm S})}{N_{\rm c}nkT}\right)} - 1 \right] - \frac{V+IR_{\rm S}}{R_{\rm ch}} \left[ 1 + a \left( 1 - \frac{V+IR_{\rm S}}{V_{\rm hr}} \right)^{-m} \right].$ (3)

Here,  $I_{ph}$  is the photocurrent,  $I_0$  is the diode reverse saturation current, V is the output voltage, k is Boltzmann's constant, T is the device temperature in K,  $R_{sh}$  is the shunt resistance, a is the fraction of ohmic current involved in avalanche breakdown, *m* is the avalanche breakdown exponent, and  $V_{\rm br}$  is the junction breakdown voltage.

#### Effect of $R_{s}$

Another numerical simulation has been performed for assessing the degradation with increasing  $R_s$ . The  $I_{mp}$  and  $V_{mp}$  of a module, with one of the 36 series-connected cells with increased  $R_s$ , were determined from the I–V curve of a module. A model of a module with an increased  $R_s$  is shown in Fig. 3, which exhibits the interconnection failure or solder bond failure



Fig. 2. Model of a module with a cell with crack. A black line shows a crack on a cell, and a dark area shows an inactive area.



as an example of increased  $R_s$ -based degradation.

Fig. 3. Model of a module with a cell with an increased  $R_s$ ; an interconnection failure is an example of degradation by increased  $R_{\rm s}$ .

### **Results and discussions**

#### Simulation of cell crack effect

The simulations of the  $I_{\rm mp}$ - $V_{\rm mp}$  curves of a crystalline silicon PV module with and without a cracked cell using Eq. (3) were carried out, as shown in Fig. 4 by the blue lines and a red line, respectively. For the cell without a crack, the cell parameters of  $I_{\rm ph} = 5.262$  A at irradiance (G) = 1 kW/m<sup>2</sup>,  $I_0 = 5.3 \times 10^{-9}$  A,  $R_s = 6.4$  mΩ/cell,  $R_{sh} = 7$  $\Omega$ /cell, n = 1.147, T = 25 °C, a = 0.1,  $V_{\rm br} = -30$  V, and m = 4 were chosen to fit the experimental data of Fig. 1. The results show that the  $I_{\rm mp}-V_{\rm mp}$  curves with a cracked cell shift toward a higher voltage as the ratio of cracked cell increases (A cracked area from 7% to 14% of the cell area). An illustration of the variation of  $I_{\rm mp}$  and  $V_{\rm mp}$  by a cracked cell is shown in Fig. 5, where one of the 36 series-connected cells was assumed to have a crack.

#### Simulation of $R_s$ effect

The simulation results with and without a cell with an increased  $R_s$  are demonstrated by the blue lines and a red line in Fig. 6, respectively. The parameters of normal cells (i.e., without an increased  $R_s$ ) were assumed to be identical to those in Fig. 4. The results suggest that an increase in  $R_s$  in the range of 0.1 - 0.6  $\Omega$  on one cell can be detected by the  $I_{\rm mp}$ - $V_{\rm mp}$  curves. An illustration of the variation of  $I_{\rm mp}$  and  $V_{\rm mp}$ 



Fig. 4.  $I_{\rm mp}$ – $V_{\rm mp}$  curves of a PV module with and without a cracked cell are represented by blue lines and a red line, respectively.





Fig. 6.  $I_{\rm mp}$ – $V_{\rm mp}$  curves of a PV module with and without an increase in  $R_s$  are represented by blue lines and a red line, respectively.



by an increase in  $R_s$  is shown in Fig. 7, where one of the 36 seriesconnected cells was assumed to have an increased  $R_s$ .

14 15 16 17 18 19 20 Voltage (V) 16 17 18 19 20 13 Voltage (V) Fig. 5. An illustration of the variation of the  $I_{\rm mp}$  and  $V_{\rm mp}$  by Fig. 7. An illustration of the variation of the  $I_{\rm mp}$  and  $V_{\rm mp}$  by the effect of cracked cell. the effect of in crease in  $R_s$ .

## Conclusion

- This method uses the new formulas corrected time-series data of  $V_{\rm mp}$  and  $I_{\rm mp}$  for temperature.
- Only the  $V_{\rm mp}$ ,  $I_{\rm mp}$ , and module temperature are necessary without other module-specific parameters, such as the TC.
- We firstly utilize the  $I_{\rm mp} V_{\rm mp}$  curve to identify a cracked cell and increase in  $R_{\rm s}$  in the PV module.
- The results are applicable to a single PV module and multiple PV modules connected in series.
- The proposed method can be flexibly applicable for various types of PV modules and systems as it uses only the  $V_{\rm mp}$ ,  $I_{\rm mp}$ , and module temperature.

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## References

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